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Giant spin-torque diode sensitivity in the absence of bias magnetic field

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Microwave detectors based on the spin-torque diode effect are among the key emerging spintronic devices. By utilizing the spin of electrons in addition to charge, they have the potential to overcome the theoretical performance limits of their semiconductor (Schottky) counterparts. However, so far, practical implementations of spin-diode microwave detectors have been limited by the necessity to apply a magnetic field. Here, we demonstrate nanoscale magnetic tunnel junction microwave detectors, exhibiting high-detection sensitivity of $75,400 \text{ mV mW}^{-1}$ at room temperature without any external bias fields, and for low-input power (micro-Watts or lower). This sensitivity is significantly larger than both state-of-the-art Schottky diode detectors and existing spintronic diodes. Micromagnetic simulations and measurements reveal the essential role of injection locking to achieve this sensitivity performance. This mechanism may provide a pathway to enable further performance improvement of spin-torque diode microwave detectors.

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The continuous progress in the development of magnetic materials and nanostructures has enabled spintronic devices with performance superior to semiconductor-based electronics, offering promising solutions for a range of future high-speed and energy-saving electronic systems^{1–7}. In particular, the spin-transfer torque^{8,9} induced by d.c. spin-polarized current can switch the magnetization^{10,11}, or excite self-oscillations^{12,13} giving rise to applications such as memories and nanoscale oscillators^{14–16}. On the other hand, microwave detectors (rectifiers) on the basis of the spin-torque diode effect can be realized when the d.c. input is replaced by a microwave current^{17,18}. The spin-torque diode effect is the result of spin-torque-induced ferromagnetic resonance (FMR), which leads to a rectification effect (that is, d.c. voltage, V_{dc}) in magneto-resistive nanoscale devices. Since its discovery¹⁷, this effect has been used for quantitative measurements of magnetic torques in magnetic tunnel junctions (MTJs) (for example, Slonczewski, field-like, and voltage-controlled torques)^{19–22}.

For practical applications in microwave detectors, the ability to obtain a device with high-detection sensitivity without using external magnetic fields, at room temperature and at low-input microwave powers is crucial. However, there are currently no practical (spintronic or conventional semiconductor) solutions that achieve all of these requirements simultaneously. In spin-torque diodes studied so far, the application of an additional external magnetic field (often canted at an angle with respect to the device plane) is required to achieve large microwave detection sensitivity^{21,23–28}. Although this external field may in principle be integrated into the device, for example, by engineering the material stack, or by using coils or permanent magnets, it is undesirable from a practical point of view due to increased size and cost of the device. On the other hand, semiconductor-based Schottky diode detectors, while not requiring a magnetic bias, fail to offer sufficient sensitivity for low input microwave powers due to the thermodynamic limit (the theoretical limit being $\sim 4,000 \text{ mV mW}^{-1}$)²⁸.

In this work, we present a spin-torque diode microwave detector meeting all of the above-mentioned requirements. This is achieved by incorporating three elements into the device. First, a perpendicularly magnetized free layer^{6,7,29}, which allows for device operation in the absence of external magnetic fields³⁰. Second, an MgO-based MTJ material stack exhibiting high-tunnel magnetoresistance (TMR). Third, the injection-locking

mechanism³¹ due to the simultaneous application of d.c. and microwave currents. The operation mechanism and the fundamental role of the injection locking are discussed on the basis of measurements combined with micromagnetic simulations.

Results

Spin-torque diode device. The devices studied in this work have an MTJ structure consisting of a synthetic antiferromagnetic $\text{Co}_{70}\text{Fe}_{30}$ (2.3 nm)/Ru (0.85 nm)/ $\text{Co}_{40}\text{Fe}_{40}\text{B}_{20}$ (2.4 nm) reference layer, exchange biased by a PtMn film, designed to have an in-plane easy axis, and a $\text{Co}_{20}\text{Fe}_{60}\text{B}_{20}$ perpendicularly magnetized free layer, separated from the reference layer by a 0.8 nm MgO tunnel barrier. A schematic of the device is shown in Fig. 1a. The free layer has an out-of-plane easy axis at zero bias field, which is realized by controlling the perpendicular magnetic anisotropy at the interface of the CoFeB layer with the MgO tunnel barrier^{6,7,29,30}. This magnetization configuration enables the device to excite large-amplitude magnetization precession under a small spin-torque³⁰. In addition, the CoFeB–MgO–CoFeB material combination ensures high TMR^{4–7}. These factors are key ingredients to enhance the sensitivity of the spin-torque diode. Electron-beam lithography and ion milling were used to fabricate the pillar-shaped devices with elliptical cross-section. All data in the main text are from one $150 \text{ nm} \times 60 \text{ nm}$ device. Other measured samples exhibited similar behaviour.

Figure 1b shows the resistance as a function of the in-plane magnetic field applied parallel to the ellipse major axis (H_{\parallel}), at a bias current of $I_{dc} = 10 \mu\text{A}$. As the field increases from $-1,000$ to $+1,000$ Oe, the resistance increases gradually as the free-layer magnetization aligns anti-parallel to the reference layer magnetization. The resistance curve scan as a function of the out-of-plane field (H_{\perp}) (inset of Fig. 1b) clearly indicates the perpendicular free layer. At zero field, a small tilting angle ($\theta = 76^\circ$) from the out-of-plane configuration is measured due to the coupling between the free and reference layers. We estimated θ , the angle between the magnetization vectors of the free layer and the reference layer, from the MTJ resistance²⁸

$$R^{-1}(\theta) = \frac{R_P^{-1} + R_{AP}^{-1}}{2} + \frac{R_P^{-1} - R_{AP}^{-1}}{2} \cos(\theta), \quad (1)$$

where the resistances in the anti-parallel (R_{AP}) and parallel (R_P) configurations are 1,200 and 640 Ω , respectively. In addition, the

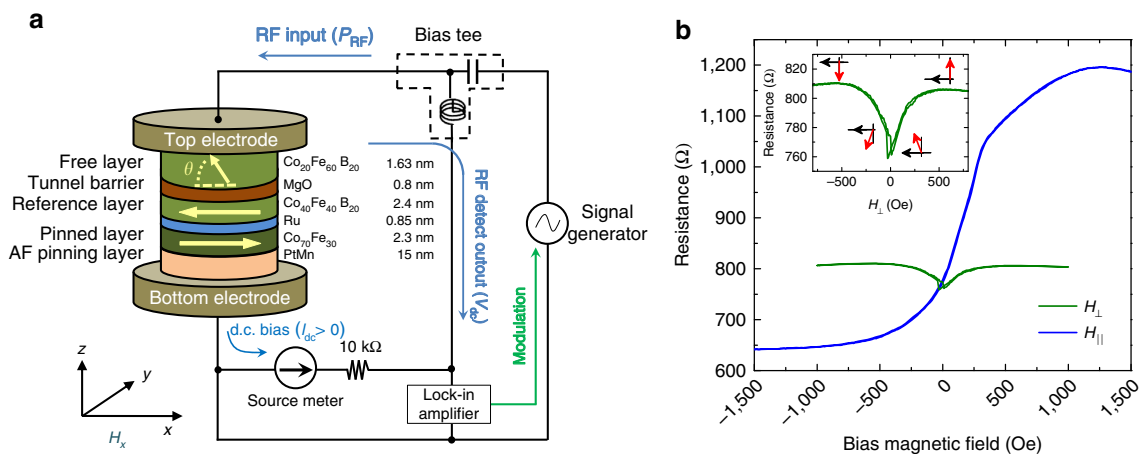


Figure 1 | Spin-torque diode device. (a) Spin-torque diode device and schematic of circuit used for FMR measurements. The device is based on an MTJ with an in-plane magnetized reference layer and a perpendicularly magnetized free layer, separated by an MgO tunnel barrier. The detected voltage (V_{dc}) is measured by a low-frequency (10 kHz) modulation method using a lock-in amplifier. (b) The magnetoresistance curve of the MTJ device under in-plane magnetic field (H_{\parallel}) and perpendicular magnetic field (H_{\perp}) for d.c. current (I_{dc}) of $10 \mu\text{A}$. The resistance scan as a function of the out-of-plane field (inset of b) clearly indicates the perpendicular free layer. The black (red) arrow denotes the magnetization direction of the reference (free) layer.

free layer exhibits a voltage-controlled interfacial perpendicular magnetic anisotropy (VCMA) estimated to be $34 \text{ fJ V}^{-1} \text{ m}^{-1}$ (see Supplementary Fig. 1 and Supplementary Note 1), in good agreement with previous reports for similar material structures^{21,22,32,33}. All measurements reported below were carried out at room temperature and zero bias magnetic field.

Detection properties. We studied the spin-torque diode response by using FMR measurements as shown in Fig. 1a (ref. 18). A weak microwave current $I_{ac} \sin(2\pi f_{ac} t)$ and a d.c. current I_{dc} were applied to the device through a bias Tee using a signal generator (E8257D, Agilent Technologies) and a source metre (2400, Keithley). At $I_{dc} = 0 \text{ mA}$, when a microwave current at a frequency f_{ac} is applied, the free layer magnetization starts to precess at the same frequency, resulting in a time-dependent resistance oscillation due to the TMR effect. As a result, a rectified voltage is generated across the MTJ¹⁷. To improve the signal-to-noise ratio, the microwave input was modulated at a low frequency (10 kHz), and the resulting rectified voltage V_{dc} was measured with a lock-in amplifier (SR830, Standard Research Systems). Figure 2a shows the measured rectified voltage as a function of the microwave frequency at $I_{dc} = 0 \text{ mA}$, for an input microwave power ranging from 3.2 to 100 nW. The maximum voltage is measured at the resonant frequency $f_0 = 1.2 \text{ GHz}$. The FMR spectra in Fig. 2a are well fitted by a sum of symmetric and antisymmetric Lorentzian functions with identical resonant frequency f_0 . The origin of the asymmetric line shape is related to the VCMA effect²¹. The detection sensitivity, defined as the rectified voltage divided by the incident microwave power (P_{RF}), that is, V_{dc}/P_{RF} , was obtained to be 970 mV mW^{-1}

(see Supplementary Fig. 2 for similar data from an additional device). This is on the same level as previously reported values (440 and 630 mV mW^{-1})^{21,28} for MTJ-based diode detectors, and at a comparable level to unbiased commercial Schottky diode detectors (500 – $1,000 \text{ mV mW}^{-1}$, Herotek, Inc.).

We next conducted spin-torque diode response studies under different d.c. bias currents. Figure 2b,c shows the detected voltage curves as a function of the microwave frequency, at a low-input microwave power of 10 nW , for the range of d.c. bias currents from -0.34 to $+0.25 \text{ mA}$. Positive d.c. currents were found to suppress the detection voltage, because in this case spin torque increases the damping of the magnetization precession, while VCMA increases the perpendicular anisotropy in the free layer. For a range of negative currents ($-0.32 < I_{dc} < -0.22 \text{ mA}$), the detection voltages were significantly enhanced and the spectra shifted to a lower frequency. Figure 2d summarizes the maximum rectified voltage (V_{max}) as a function of d.c. bias current, while the inset of Fig. 2d shows the spectral linewidth of the spin-torque FMR data, with the indication of the region where the larger detection voltage is measured. As discussed later in detail, this corresponds to the current region where the injection locking is achieved.

Figure 3a shows the detection voltage as a function of P_{RF} for various d.c. bias currents. The device shows a quadratic detection dependence on the d.c. bias, consistent with a previous study²⁸. Moreover, a large detection voltage ($\sim \text{mV}$ order) is achieved for small input power. For example, the maximum detected voltage reaches $754 \mu\text{V}$ at $I_{dc} = -0.25 \text{ mA}$ and $P_{RF} = 0.01 \mu\text{W}$, which is about $80 \times$ larger than the one measured at zero bias current. The corresponding detection sensitivity of $75,400 \text{ mV mW}^{-1}$ is substantially larger than state-of-the-art biased Schottky diode

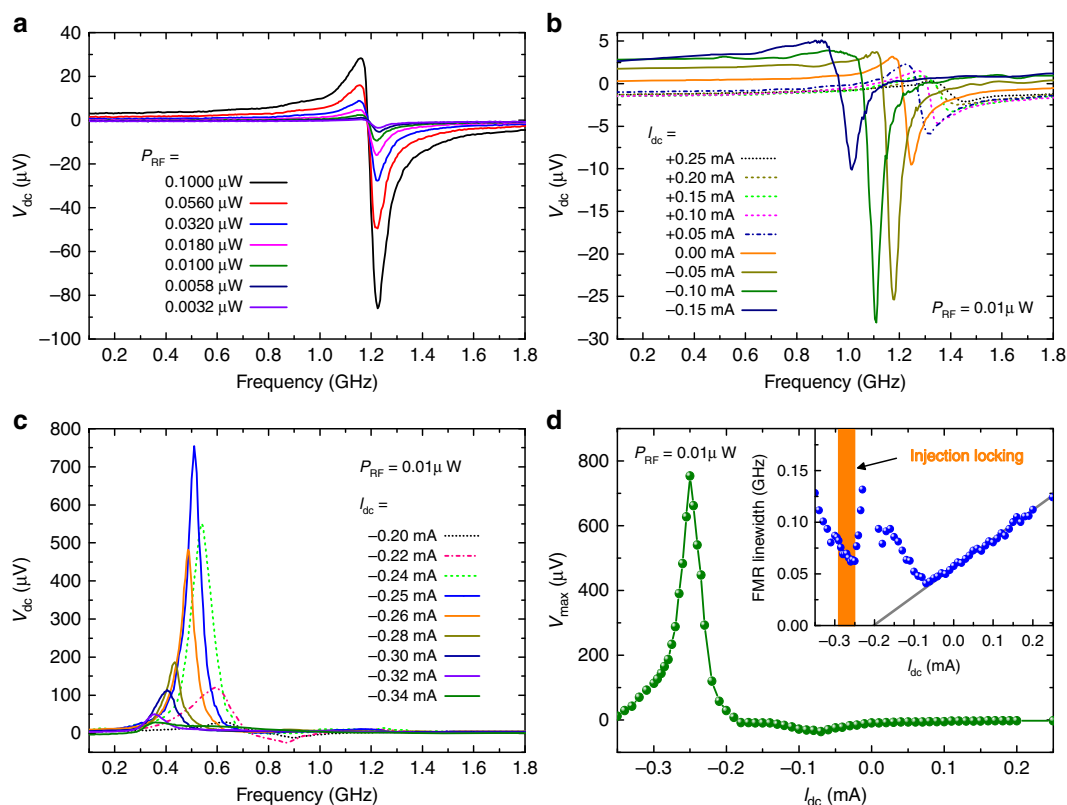


Figure 2 | Voltage detection characteristics of spin-torque diode device. (a) Detection voltage (V_{dc}) as a function of microwave frequency, for various input microwave powers (P_{RF}) at zero d.c. bias current. (b,c) V_{dc} as a function of microwave frequency under various d.c. bias currents (I_{dc}). The d.c. bias was found to significantly affect V_{dc} . (d) Maximum V_{dc} as a function of the d.c. bias. The inset in d shows the spectral linewidth of the free-layer FMR as a function of I_{dc} . By extrapolating the fitting line (grey solid line), the critical current (I_c) for magnetization stability in the free layer is estimated to be -0.2 mA .

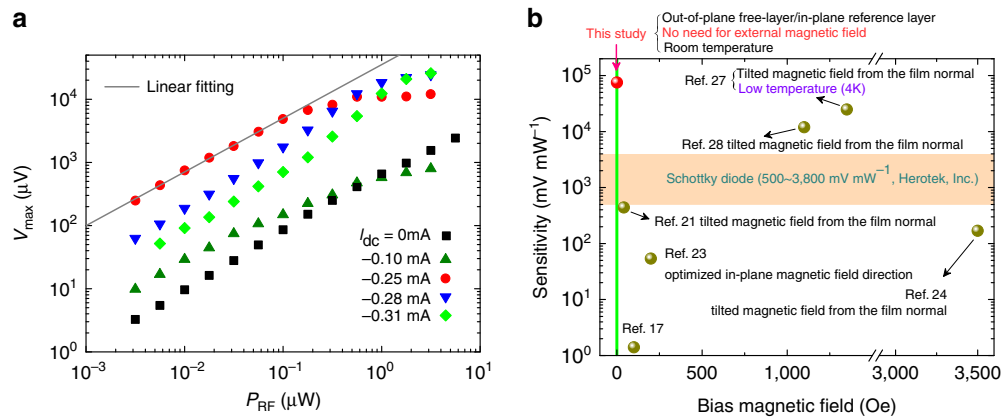


Figure 3 | RF power dependence and the comparison of detection sensitivity with the indication of the required bias field. (a) The dependence of output voltage on the RF input power under different d.c. bias current (I_{dc}) values. (b) The detection sensitivity values reported previously require an external magnetic field with a particular direction and amplitude, while in this study the giant sensitivity is achieved in the absence of any bias magnetic field.

detectors ($3,800 \text{ mV mW}^{-1}$, Herotek, Inc.) and the best existing spintronic diodes ($12,000 \text{ mV mW}^{-1}$), which additionally require large magnetic bias fields for their operation²⁸. Figure 3b compares our results with previously reported detection sensitivities for different spin-torque diodes, with the indication of the required external magnetic field. It can be observed that the devices reported in this work represent the combination of high-detection sensitivity and bias-field-free operation. In addition, the device exhibits signal-to-noise ratio, which is of the same order as those of previous reports²⁸ (see Supplementary Note 2 and Supplementary Figs. 3,4,5). It is worth noting that the giant detection sensitivities observed here are not only substantially larger than those of Schottky diodes, but they are also achieved at low microwave input power ($< 100 \text{ nW}$). By comparison, Schottky diodes typically do not provide satisfying microwave-to-d.c. conversion efficiency for sub- μW input microwave power³⁴. Furthermore, the spin-torque diode devices can be scaled down to nano-metre size ($0.07 \mu\text{m}^2$ in this study), which makes them potentially suitable for compact on-chip microwave detectors.

Discussion of physical mechanism. We next focus on the mechanisms responsible for the large-voltage detection sensitivity. Under d.c. bias, two previous experiments demonstrated that the detection voltage can be enhanced due to the nonlinear FMR^{27,28}. In thermally assisted nonlinear FMR²⁷ (or stochastic resonance), an applied radiofrequency (RF) current excites a large-amplitude precession with the assistance of thermal energy, and the detection voltage shows an exponential dependence on the RF input power. Another type of nonlinear FMR (called nonlinear FMR with asymmetric potential), in which the large detection voltage is linked to a rotation of the orbital centre of the free-layer magnetization, has been also observed²⁸. The maximum detection voltage is achieved near $I_{dc} = I_c$, where I_c is the critical current at which the equilibrium configuration of the magnetization is destabilized by the spin-transfer torque²⁸. By comparison, the device discussed in this article, exhibits quadratic detection properties for small RF input power (see Fig. 3a), and enhanced detection voltage in the specific range from -0.22 to -0.32 mA (see Fig. 2d), which is above I_c . Here, I_c is estimated to be -0.2 mA , from the extrapolation of the fitted line in the d.c. current dependence of the FMR spectral linewidths, as shown in the inset of Fig. 2d. Hence, the underlying physics in this study is different from that of nonlinear FMR observed in previous experiments.

An alternative mechanism is the theory related to the out-of-plane precession³⁵, in which the device operates as a non-resonant broadband microwave detector, and the output voltage is virtually independent of the input microwave power. The device discussed here exhibits a resonant character (see Fig. 2b,c), and the output voltage depends on P_{RF} (see Fig. 3a). Hence, the mechanism driving the large detection sensitivity in this study is different from this picture as well.

Role of injection locking on detection behaviour. To gain a deeper understanding of the ultrahigh sensitivity mechanism, we performed micromagnetic simulations (see Methods). Our computational results show persistent magnetization dynamics (self-oscillations) (at $I_{ac} = 0 \text{ mA}$), as well as injection locking (at $I_{ac} > 0 \text{ mA}$)^{31,36–38}. Figure 4a shows an example of the detection voltage as a function of frequency (f_{ac}), as computed by means of micromagnetic simulations for $I_{dc} = -0.26 \text{ mA}$ and $I_{ac} = 7 \mu\text{A}$ ($P_{RF} = 0.15 \mu\text{W}$). The large detection voltage is observed in the frequency range corresponding to the locking region (between 510 and 540 MHz), as shown in Fig. 4b, where it can be clearly observed that the microwave emission frequency f_p is locked to the frequency f_{ac} of the input microwave current. Within the locking region, an intrinsic phase shift Φ_s (ref. 39) exists between the oscillation resistance and the microwave current. The origin of Φ_s can be understood from the theory developed in ref. 40, in which it is directly linked to the coupling between the amplitude and the frequency of the self-oscillation (see equation (56) in ref. 40). It is noted that the value of Φ_s inside the locking bandwidth depends on the microwave frequency (Fig. 4c), similar to that in a previous study⁴¹. Figure 4d shows a comparison between the experimental and theoretical values for the frequency f_0 of the maximum rectification voltage, as a function of the d.c. bias current. The simulation data (open circles) are quantitatively consistent with the experimental data (olive colour), namely, a red shift is observed in the frequency f_0 with increasing the amplitude of the negative current, along with a frequency jump of about 300 MHz. This analysis points to a scenario where the injection locking is responsible for the observed giant detection sensitivity.

To further verify the role of the injection locking, we conducted additional experiments to study the current-induced microwave emission¹² with and without a RF input in our samples, recorded using a 9 kHz–26.5 GHz spectrum analyzer (see Supplementary Fig. 6). The output of microwave emissions in the absence of P_{RF}

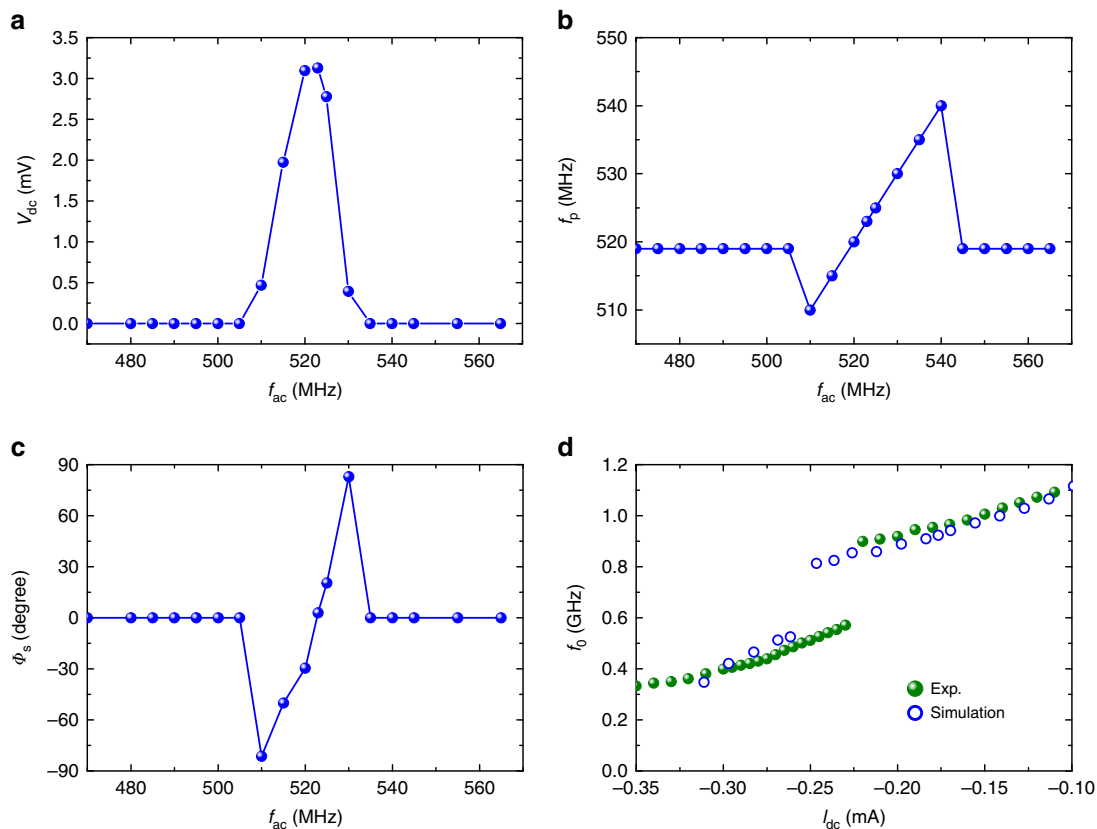


Figure 4 | Micromagnetic simulations. (a) Rectified voltage and (b) Oscillation frequency (f_p) of the microwave emission, as a function of the input microwave frequency (f_{ac}). (c) Intrinsic phase shift between the microwave current and the oscillating TMR signal. The results of micromagnetic simulations are obtained for d.c. bias currents $I_{dc} = -0.26$ mA and microwave current $I_{ac} = 7$ μ A. (d) A comparison between the experimental and simulated resonant frequency (f_0) of the maximum detection voltage as a function of I_{dc} .

as a function of I_{dc} is shown in Fig. 5a. The oscillation frequency (f_p) exhibits a red shift with increasing the bias current. The frequency jump in the f_p versus I_{dc} response is related to the sign change of the x -component of the oscillation axis from negative to positive, as also indicated from the change in the resistance curve (see Fig. 5d). Similar behaviour was also observed in spin-torque oscillators at low out-of-plane bias fields⁴². Near $I_{dc} = -0.34$ mA, the steady magnetization dynamics are switched off, analogous to the disappearance of the detection spectrum in the spin-torque diode measurements (see Fig. 2c). Figure 5b shows the analogous data when an RF drive $P_{RF} = 1$ μ W at 480 MHz is added to I_{dc} . At $I_{dc} = -0.25$ mA the oscillation frequency locks to the drive frequency, and the locking continues up to $I_{dc} = -0.29$ mA. At larger bias currents the oscillation frequency is unlocked from the drive frequency. In the locking range, the linewidth of the microwave emission is significantly narrowed by a factor of $8 \times$ (to 15 MHz), as can be observed in Fig. 5c, but is still much larger than the linewidth of the external microwave signal (on the order of several Hertz). These results indicate that the frequency-locking does not always result in a full phase-locking of the spin-torque nano-oscillator to the external microwave signal, consistent with previous reports^{37,38}. This can be attributed to the influence of noise^{37,38,43}, that is, the external microwave signal has to compete with noise, which results in fluctuations of the oscillator phase.

Despite full phase-locking not being reached, the detection voltage V_{dc} is drastically increased as shown in Fig. 5e. Quantitatively, for a fixed frequency, the detection voltage is given by $V_{dc} = \frac{1}{2} I_{ac} \Delta R_s \cos(\langle \Phi_s \rangle) + I_{dc} \Delta R_{dc}$ (refs 27,28), where $\Delta R_{dc}(I_{ac}) = R_{dc}(I_{ac}) - R_{dc}(0)$ is the difference between the average

resistance in the presence and in the absence of I_{ac} , while $\langle \Phi_s \rangle$ is the time-average intrinsic phase shift, and ΔR_s is the amplitude of the oscillating resistance in the presence of both I_{dc} and I_{ac} . It is worth pointing out that the value of ΔR_s can be significantly larger in the presence of d.c. bias, given that it results from the amplitude of the self-oscillation of the magnetization, rather than conventional FMR. As an example, for $I_{dc} = -0.26$ mA and $I_{ac} = 18$ μ A ($P_{RF} = 1$ μ W, $f_{ac} = 480$ MHz), from Fig. 5d $\Delta R_{dc}(I_{ac}) = 60$ Ω , while from the output power (Fig. 5b) it can be estimated that the oscillation is due to 30% of the total TMR signal, which corresponds to $\Delta R_s = 170$ Ω . Considering $\langle \Phi_s \rangle \approx 0$, the calculated detection voltage of ~ 17.13 mV is consistent with the measurements in Fig. 5e. From a theoretical point of view, according to the above analysis the detection voltage is limited by the maximum TMR signal. In Fig. 5f, the locking range is more explicitly shown as a function of the RF drive amplitude. The locking range is deduced from the dependence of the oscillation frequency f_p on the drive frequency f_{ac} , where the microwave emission is locked to the injected signal (see Fig. 4b for simulation results, or Supplementary Note 3 and Supplementary Fig. 7 for additional experimental data). The locking range increases with the drive amplitude, which is consistent with the simulation data and in agreement with the analytical theory⁴⁰.

Discussion

In summary, we have demonstrated giant sensitivity of nanoscale spintronic diodes in the absence of any external magnetic field, at room temperature and for low-input microwave power. The analysis of microwave emission measurements with and

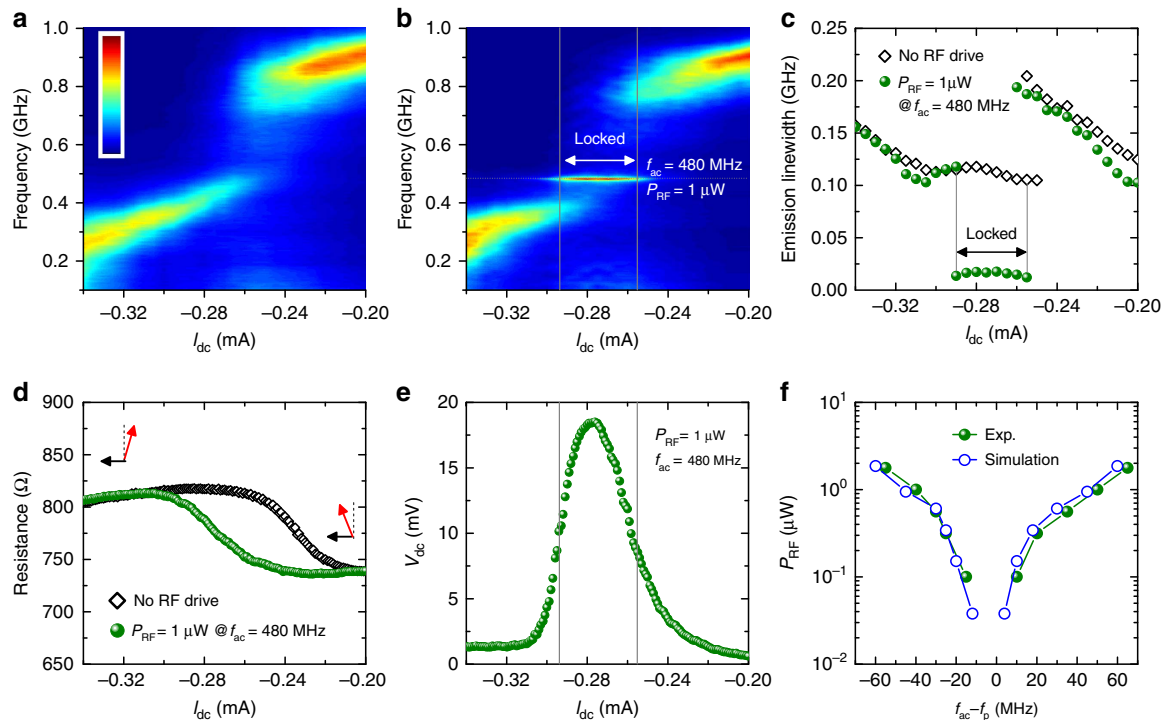


Figure 5 | Injection locking of spin-torque microwave emission to an external microwave signal. (a) Plot of spin-torque microwave emission spectra as a function of d.c. bias currents I_{dc} , with amplitude shown in a linear colour scale from 0 (blue) to 40 nW GHz^{-1} (red). (b) Same as a but with a RF drive at 480 MHz and RF power $P_{RF} = 1 \mu\text{W}$. (c) Spectral linewidth of microwave emission as a function of I_{dc} , with/without a RF drive deduced from a and b. (d) Device resistance as a function of I_{dc} with and without the RF drive. The precession axis of the free-layer magnetization (red arrows) and reference layer polarization (black arrows) are also indicated. (e) The detected voltage V_{dc} as a function of I_{dc} . Vertical lines indicate the region of locking. (f) A comparison between experimental values (olive dots) and micromagnetic calculations (blue circles) of the locking range as a function of RF drive amplitude, at $I_{dc} = -0.26 \text{ mA}$.

without RF input, as well as micromagnetic simulations, reveal that injection locking is the key mechanism to achieve this large sensitivity. It is anticipated that this mechanism may provide a pathway for development of high-performance spintronic microwave detectors.

Methods

Sample preparation. The continuous multilayer thin films with stacks of composition PtMn (15)/Co₇₀Fe₃₀ (2.3)/Ru (0.85)/Co₄₀Fe₄₀B₂₀ (2.4)/MgO (0.8)/Co₂₀Fe₆₀B₂₀ (1.63) (thickness in nm) were deposited using a Singulus TIMARIS physical vapour deposition system and annealed at 300 °C for 2 h in a magnetic field of 1 T. The films were subsequently patterned into ellipse-shaped pillars using optical and electron-beam lithography combined with ion milling. The resistance-area product in the parallel magnetization configuration was $4.5 \Omega \mu\text{m}^2$, and the in-plane TMR ratio, defined as $(R_{AP} - R_P)/R_P$, was 87.5%.

Micromagnetic simulations. We numerically solve the Landau–Lifshitz–Gilbert–Slonczewski equation which includes the field-like torque T_{OP} (refs 44,45), and the voltage dependence of the anisotropy, that is, VCMA²¹. The T_{OP} is considered to be dependent on the square of the bias voltage up to a maximum value of 10% of the in-plane torque, computed for a current density $|J| = 4.0 \times 10^6 \text{ A cm}^{-2}$ (ref. 19). However, our simulations show that the field-like torque term does not qualitatively influence the detection voltage, as already observed in the scenario of ref. 21. The total torque, including also the in-plane component T_{IP} is given by

$$T_{IP} + T_{OP} = \frac{g}{|e| \gamma_0 M_s^2 t} \mu_B J(\mathbf{m}, \mathbf{m}_p) g_T(\mathbf{m}, \mathbf{m}_p) \left[\mathbf{m} \times (\mathbf{m} \times \mathbf{m}_p) - q(V)(\mathbf{m} \times \mathbf{m}_p) \right], \quad (2)$$

where g is the gyromagnetic splitting factor, γ_0 is the gyromagnetic ratio, μ_B is the Bohr magneton, $q(V)$ is the voltage-dependent parameter for the perpendicular torque, $J(\mathbf{m}, \mathbf{m}_p)$ is the spatially nonuniform current density, V is the voltage (computed from $I_{dc} - R$ curves, see Fig. 5d), t is the thickness of the free layer, and e is the electron charge. The effective field takes into account the standard micromagnetic contributions (exchange, self-magnetostatic) as well as the Oersted field due to both microwave and d.c. currents. The presence of the VCMA has been modelled as an additional contribution to the effective field. The parameters used

for the CoFeB are saturation magnetization $M_s = 9.5 \times 10^5 \text{ A m}^{-1}$, exchange constant $A = 2.0 \times 10^{-11} \text{ J m}^{-1}$, and damping parameter $\alpha = 0.02$. The zero bias anisotropy constant $k_u = 5.52 \times 10^5 \text{ J m}^{-3}$ has been estimated from the fitting of the FMR frequency $f_0 = 1.245 \text{ GHz}$ from Fig. 2a, while the VCMA coefficient is $34 \text{ fJ V}^{-1} \text{ m}^{-1}$ (see Supplementary Note 1). The minimum value of the k_u achieved at $I_{dc} = -0.35 \text{ mA}$ is $5.45 \times 10^5 \text{ J m}^{-3}$. The polarization function $g_T(\mathbf{m}, \mathbf{m}_p) = 2\eta_T(1 + 2\eta_T^2 \mathbf{m} \cdot \mathbf{m}_p)^{-1}$, where \mathbf{m} and \mathbf{m}_p are the normalized magnetizations of the free and pinned layers, has been computed by Slonczewski^{46,47}. We have used for the spin-polarization η_T the value 0.6 (ref. 19).

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Author contributions

B.F., Z.M.Z., G.F. and H.W.J. initiated this work. P.K.A. and I.N.K. designed the MTJ devices. J.L. and B.O. deposited the films, and J.A.K. fabricated the devices. B.F. and X.J.H. performed the measurements, M.C. and G.F. performed micromagnetic simulations. Z.M.Z. and G.F. analysed the data and wrote the paper with contributions from P.K.A. All authors contributed to the discussion and commented on the manuscript.

Additional information

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